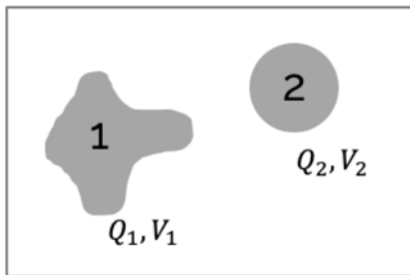




**Carga** y **potencial** de un sistema de conductores

$$q = C V$$



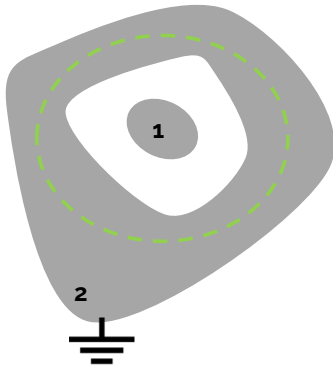
$$Q_1 = C_{11}V_1 + C_{12}V_2$$

$$Q_2 = C_{21}V_1 + C_{22}V_2$$

$$C_{mn}$$

$m = n$	Coefficientes de <b>capacidad</b> de los conductores en el sistema	$> 0$
$m \neq n$	Coefficientes de <b>inducción</b> de los conductores en el sistema	$< 0$
$C_{mn} = C_{nm}$		

## Carga y potencial de un sistema de **dos** conductores



$$Q_1 = C_{11}V_1 + C_{12}V_2$$

$$Q_2 = C_{21}V_1 + C_{22}V_2$$

$$Q_1 = C_{11}V_1$$

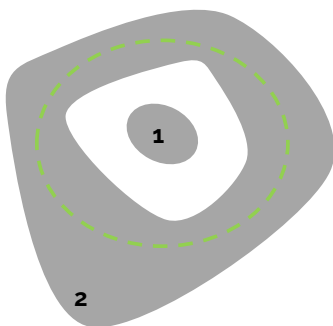
$$Q_2 = C_{21}V_1 = -Q_1$$

Capacidad de un capacitor  
(sistema de dos conductores  
donde uno rodea al otro)

$$C = C_{11} = -C_{21}$$

## Carga y potencial de un sistema de **dos** conductores

$$C = C_{11} = -C_{21}$$



$$Q_1 = C V_1 - C V_2$$

$$Q_2 = -C V_1 + C_{22}V_2$$

$$Q_1 = C (V_1 - V_2)$$

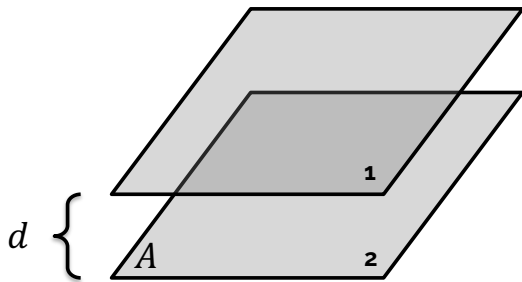
$$Q_2 = -C V_1 + C_{22}V_2$$

$$Q_2 = -Q_1 + C' V_2$$

$$C' = C_{22} - C$$

## Capacitor plano

$$Q_1 = C (V_1 - V_2)$$

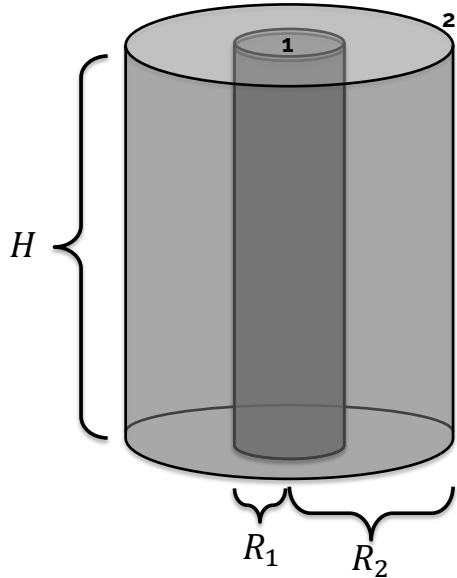


$$C = \frac{Q_1}{V_1 - V_2} = \frac{\epsilon_0 A}{d}$$

**PHET**  
INTERACTIVE SIMULATIONS



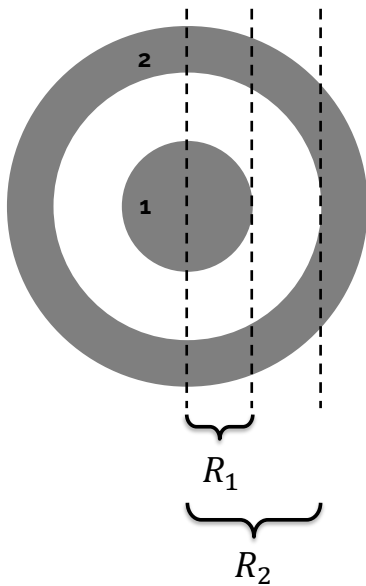
## Capacitor cilíndrico



$$Q_1 = C (V_1 - V_2)$$

$$C = \frac{Q_1}{V_1 - V_2} = \frac{2\pi \epsilon_0 H}{\log R_2/R_1}$$

## Capacitor esférico

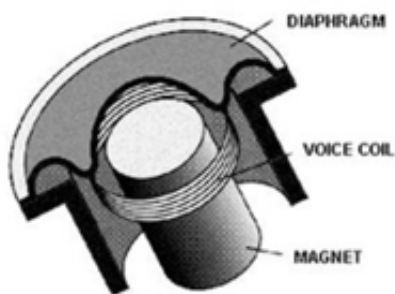


$$Q_1 = C (V_1 - V_2)$$

$$C = \frac{Q_1}{V_1 - V_2} = \frac{4\pi \epsilon_0}{\left(1/R_1 - 1/R_2\right)}$$

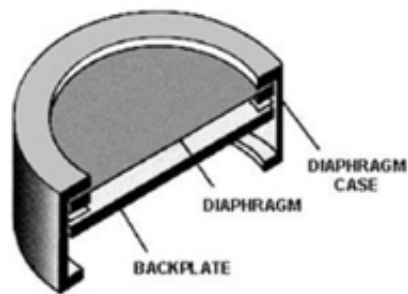


Micrófonos: ondas de presión a voltaje/corriente



**Dynamic**

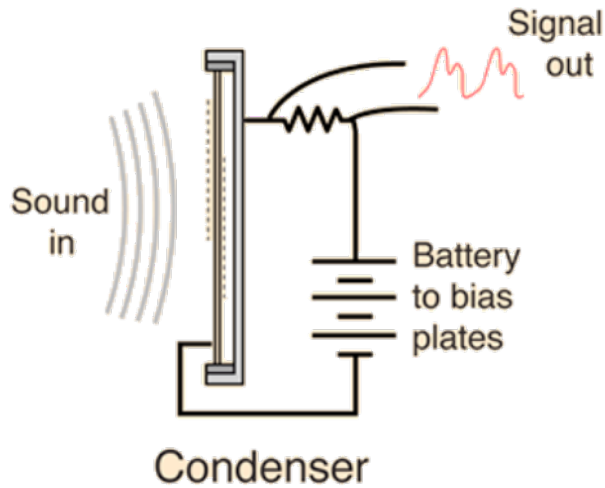
**Unidad 5/6**



**Condenser**

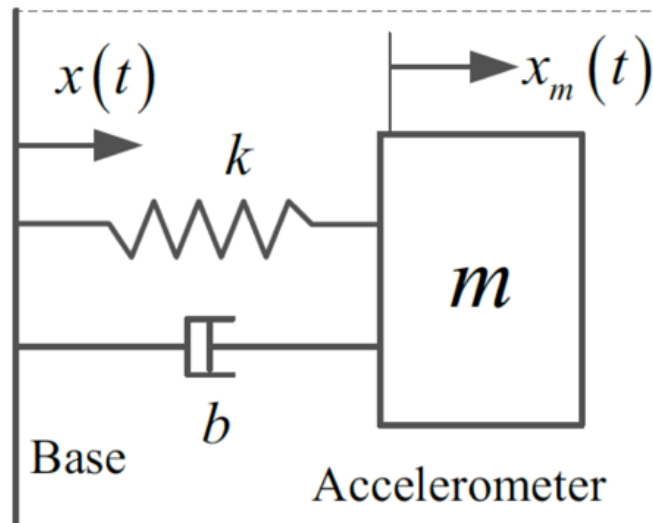
**Unidad 2/3**

## El micrófono condensador



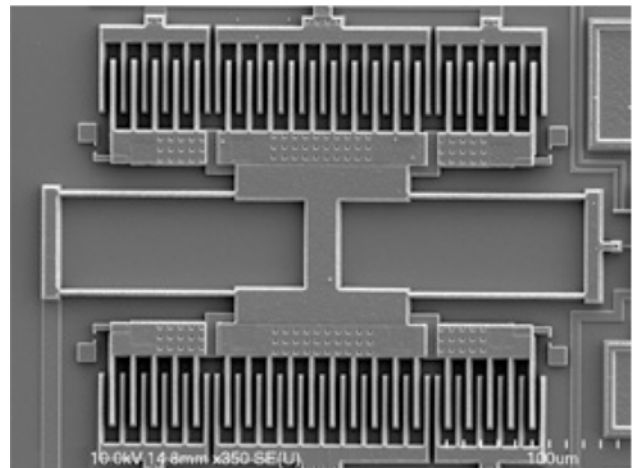
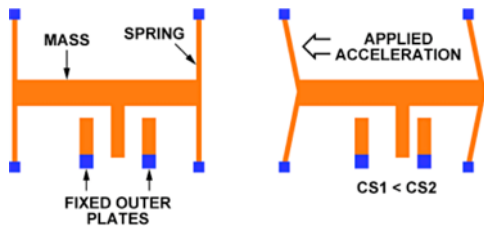
Most modern measurement microphones are pressure-sensing condenser microphones. Their principle of operation, which was invented by E. C. Wente in 1917 [1], is based on variation of the distance, and thereby the capacitance, between a moveable and a stationary plate, which are electrically conducting and form a capacitor. A stretched diaphragm that is typically  $2\text{--}8\ \mu\text{m}$  thick is mounted at one end of the, generally cylindrical, microphone body. This diaphragm constitutes the plate that is displaced by the sound pressure, while the stationary, parallel plate, called the back-plate, is placed behind it, inside a closed cavity. The distance between the plates, at rest, is typically  $15\text{--}25\ \mu\text{m}$ ; see Figure 1a and b. The capacitance is from about 3 to 70 pF, depending on the diameter of the microphone, which, for the common models, is in the range between 3 and 24 mm.

## Acelerómetro



# Acelerómetro **capacitivo**

MEMS: Micro-electromechanical systems



# Acelerómetro **capacitivo**



Samsung Galaxy Note 3



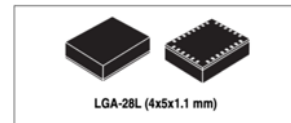
## LSM330DLC

iNEMO inertial module:  
3D accelerometer and 3D gyroscope

Datasheet — production data

### Features

- Analog supply voltage: 2.4 V to 3.6 V
- Digital supply voltage IOs: 1.8 V
- Low power mode
- Power-down mode
- 3 independent acceleration channels and 3 angular rate channels
- $\pm 2 g/\pm 4 g/\pm 8 g/\pm 16 g$  dynamically selectable full scale
- $\pm 250/\pm 500/\pm 2000$  dps dynamically selectable full scale
- SPI/I<sup>2</sup>C serial interface (16-bit data output)
- Programmable interrupt generator for free-fall and motion detection
- ECOPACK<sup>®</sup> RoHS and "Green" compliant

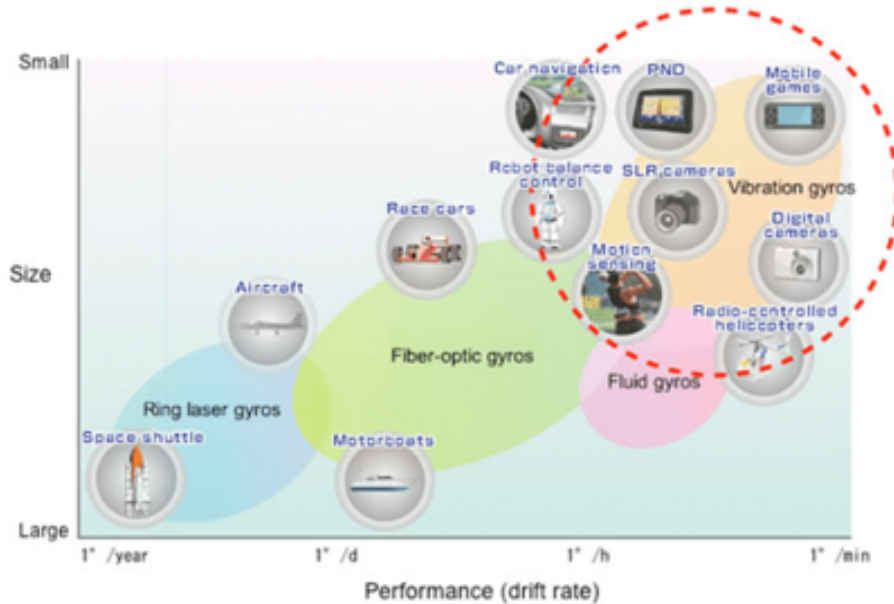


The various sensing elements are manufactured using specialized micromachining processes, while the IC interfaces are developed using a CMOS technology that allows the design of a dedicated circuit which is trimmed to better match the sensing element characteristics.

The LSM330DLC has dynamically user-selectable full scale acceleration range of  $\pm 2 g/\pm 4 g/\pm 8 g/\pm 16 g$  and angular rate of  $\pm 250/\pm 500/\pm 2000$  deg/sec.

At steady state the nominal value of the capacitors are few pF and when an acceleration is applied the maximum variation of the capacitive load is in fF range.

## Giróscopo



## Giróscopo resonante: Coriolis

$$\vec{v}_I = \vec{v}_R + \vec{\Omega} \times \vec{r}$$

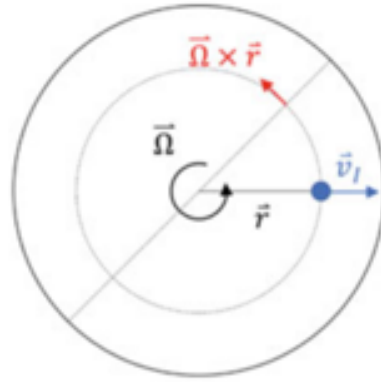
$$\begin{aligned} \vec{a}_I &= \left( \frac{d^2 \vec{r}}{dt^2} \right)_I = \left[ \left( \frac{d}{dt} \right)_R + \vec{\Omega} \times \right]^2 \vec{r} \\ &= \left( \frac{d^2 \vec{r}}{dt^2} \right)_R + 2\vec{\Omega} \times \left( \frac{d\vec{r}}{dt} \right)_R + \vec{\Omega} \times (\vec{\Omega} \times \vec{r}) \\ &= \vec{a}_R + 2\vec{\Omega} \times \vec{v}_R - \Omega^2 \vec{r} \end{aligned}$$



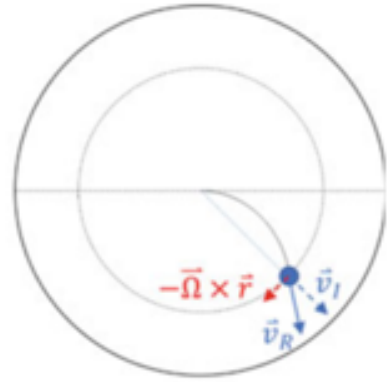
# Giróscopo resonante: Coriolis



$t = 0$

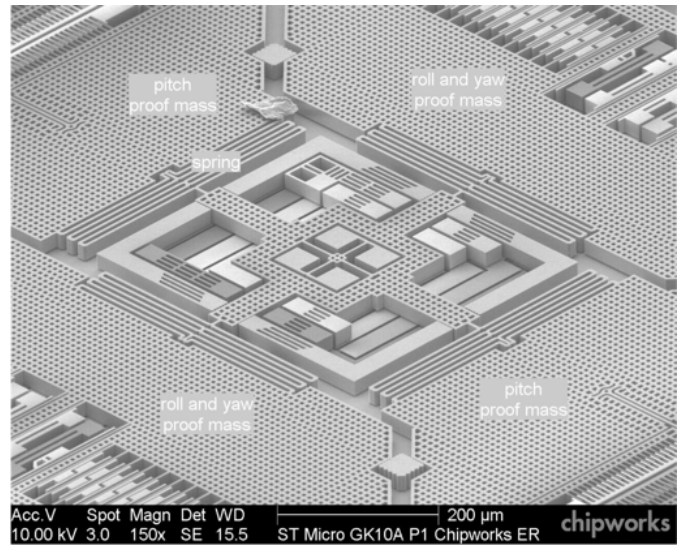
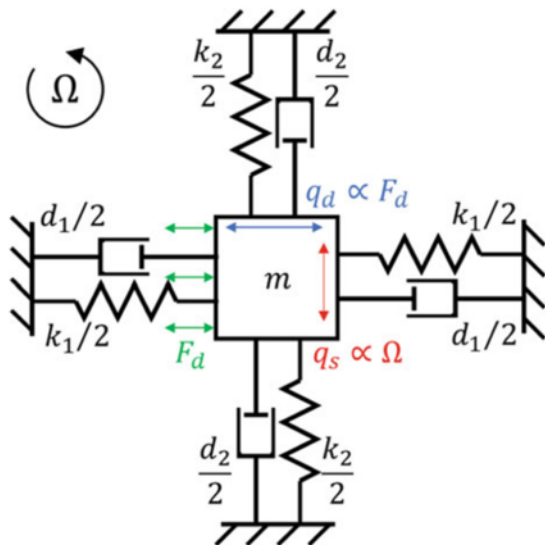


Sistema Inercial  
( $t > 0$ )



Sistema Rotante  
( $t > 0$ )

# Giróscopo resonante: Coriolis





$$Q_1 = C (V_1 - V_2)$$